Moving layers and interfaces : a thermodynamical approach of Wear Contact

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Loss of sound material is due to wear.

Friction - contact between bodies - interface propagation

Essai de video essai de vidéo



Model of damage - Dissipation - Global behaviour of the interface Ω_3 $\Omega_3 = Sxh$: detached particles, damaged media, fluids: complex behaviour Integration over the thickness: constitutive equation for the interface S

Moving interface / moving layer

Material characteristics change :

- Brutal transition : moving interface and discontinuities
- Continuous Transition : moving layer and continuous damage laws.

Moving interface and Transformation of material

Material 1 is changed in material 2 along a moving interface

the mass flux is the loss of sound material.

Preliminaries



$$F = \int_{a}^{b} f(x,t) dx$$
$$= \int_{a}^{\Gamma(t)} f(x,t) dx + \int_{\Gamma(t)}^{b} f(x,t) dx$$



Γ

$$\dot{F} = \int_{a}^{b} \dot{f} \, dx + \left(f(\Gamma^{+}, t) - f(\Gamma^{-}, t) \right) \dot{\Gamma}$$

$$[f]_{\Gamma} = f(\Gamma^+, t) - f(\Gamma^-, t)$$

Propagation of interface

 \Rightarrow jump conditions.



Each medium is linear elastic : x proportion of phase 2

Equilibrium :

$$\sigma = E_1 \varepsilon_1 = E_2 \varepsilon_2 = \Sigma, \quad u(0) = 0$$

Energy :

$$W(\sigma, x) = -\frac{1}{2}\sigma^2(\frac{x}{E_2} + \frac{1-x}{E_1})$$

Energy release rate

$$G = -\frac{\partial W}{\partial x} = \frac{1}{2}\sigma^2(\frac{1}{E_2} - \frac{1}{E_1}); \quad D_m = G\dot{x}$$

Preliminaries



Quasicrack : antiplane shear conditions

$$K^{2} = h \frac{\tau_{o}^{2}}{\alpha + 1} \left[\left(\frac{R_{m}}{R_{o}} \right)^{\alpha + 1} + \frac{\alpha - 1}{2} \right]$$

Neuber (1969), Bui-Ehrlacher (1978), Stolz (2010).



Interpretation

$$D_{\Gamma} = \mathcal{G} \phi, \quad m = \rho \phi$$

Then

 $m=0, \mathrm{no}\ \mathrm{loss}\ \mathrm{of}\ \mathrm{sound}\ \mathrm{material}\ \Rightarrow\ \mathrm{no}\ \mathrm{wear}$

$$\begin{cases} \mathcal{G}(X,t) < G_c, & \phi = 0\\ \mathcal{G}(X,t) = G_c, & \phi \ge 0 \end{cases}$$

friction
$$D_3 = \int_h d_m \, dz = \int_h (\boldsymbol{\sigma} : \dot{\boldsymbol{\varepsilon}} - \dot{w_3}) \, dz$$

Moving Layer

The material is described with continuous damage

In
$$\Omega$$
 free energy : $w(\varepsilon, d, \alpha) = (1 - d)w_o(\varepsilon, \alpha) + H(\alpha)$

$$Y = -\frac{\partial w}{\partial d}, \quad A = -\frac{\partial w}{\partial \alpha}$$

d varies from 0 to 1, no discontinuities.

$$d_m = Y\dot{d} + A\dot{\alpha}$$

Dissipation



but in the moving frame

$$f(x,t) = f(x - \phi t \underline{n}, t) \quad \dot{f} = -\phi \nabla f \underline{n} + D_{\phi} f$$

1-D Example :



Free energy : $W = \frac{1}{2} E(d) \varepsilon^2$

Matching Conditions $E(0) = E_1, E(1) = E_2$

Total Dissipation under steady-state condition $(\dot{d}+\phi\nabla d.\underline{n}=0)$

$$D_m = \phi \int_h \frac{1}{2} \sigma^2 (-\frac{E'}{E^2}) \nabla d \, \mathrm{d}z = \phi \frac{1}{2} \sigma^2 \int_1^0 (-\frac{E'}{E^2}) \mathrm{d}d = G\phi$$

Dissipation with moving layer

$$D_m = \phi \int_h (Y\nabla d + A\nabla\alpha) dz + \int_h (YD_\phi d + AD_\phi\alpha) dz$$

that is

$$D_m = \bar{G}\phi + \int_h d_\phi \ dz$$

Steady-state motion : the last term is zero.

$$\bar{G} = \int_{h} (Y\nabla d + A\nabla\alpha) dz \le hY_c$$

Geometry of the layer, Curvature tensor : $\nabla \underline{n}.\underline{a}_{\alpha} = -b_{\alpha}^{\beta}\underline{a}_{\beta}$



$$dS_i = \det(b \pm_i h \mathbf{I}) = j_i \, dS$$
$$\int_B f \, d\Omega = \int_{\Gamma} (\int_h f j(z) dz) \, dS = \int_{\Gamma} f_S \, dS$$

Eshelby momentum tensor

$$\boldsymbol{P} = w \mathbf{I} - \boldsymbol{\sigma} \cdot \nabla \underline{u}$$

Then

$$\operatorname{div} \boldsymbol{P}^T = -Y\nabla d - A\nabla \alpha$$

Introducing the relative coordinate

$$\underline{x} = \underline{X}_{S} + \underline{z}\underline{n}, \quad D_{\phi} \underline{x} = \phi \underline{n} + z \nabla \phi$$
$$\int_{\Gamma} \bar{G}\phi(s) \, \mathrm{d}S = -\int_{B} \mathbf{P} : \nabla (D_{\phi} \underline{x}) \, \mathrm{d}\Omega + \int_{\Gamma_{i}} \underline{n} \cdot \mathbf{P} \cdot D_{\phi}(\underline{x}) j_{i} \, \mathrm{d}S$$



$$\bar{G}_i(s) = \left(\int_{h_i} (Y\nabla d + A\nabla\alpha)j \, \mathrm{d}S\right) \cdot \underline{n}(s)$$



$$\psi_s \rho_s = \int_h w(\boldsymbol{\varepsilon}, \alpha)_z \rho_z j(z) \, \mathrm{d}z$$
$$D_s \rho_s = \int_h D(\dot{\boldsymbol{\varepsilon}}, \dot{\alpha})_z \rho_z j(z) \, \mathrm{d}z$$

Dissipation associated with the interface

Total potential energy : $\int_{\Omega} w \rho \ \mathrm{d}\Omega + \int_{\Gamma} \psi_s \rho_s \ \mathrm{d}S$

$$D_{m} = \int_{\partial\Omega} \underline{n} \cdot \boldsymbol{\sigma} \cdot \underline{v} \, \mathrm{d}\Omega - \frac{\mathrm{d}}{\mathrm{d}t} \left(\int_{\Omega_{i}} w_{i} \rho_{i} \, \mathrm{d}\Omega + \int_{\Gamma} \rho_{s} \psi_{S} \, \mathrm{d}S \right)$$

$$= \int_{\Gamma} \left(-\boldsymbol{\sigma}_{i} : [\boldsymbol{\varepsilon}_{i}]_{\Gamma} + \rho_{i} (w_{i} - \psi_{S})) j_{i} \phi_{i} \, \mathrm{d}S$$

$$+ \int_{\Gamma} \frac{\partial \mathrm{D}_{S}}{\partial \underline{v}_{i}} \cdot \mathcal{D}_{\phi} \underline{u}_{i} + \frac{\partial \mathrm{D}_{S}}{\partial \alpha} \cdot \mathcal{D}_{\phi} \alpha + Q \cdot \mathcal{D}_{\phi} \rho_{s} \, \mathrm{d}S$$

The mass density is an internal parameter for the interface.

The behaviour of the layer

 $\text{Main idea}: -h \leq z \leq h$

$$\underline{u}_3(X_S, z) = \underline{u}^o(X_S) + z\underline{u}^1(X_S) + \dots$$

Continuity of displacement

$$u_1 = \underline{u}_3(X_s, h), \quad u_2 = \underline{u}_3(X_s, -h)$$

Then

$$w(X_s) = u_1 - u_2 = 2h\nabla \underline{u} \cdot \underline{n}, \quad \underline{u}^o = \frac{1}{2}(\underline{u}_1 + \underline{u}_2) + o(h^2)$$

Introducing these asymptotic expansion in global potential for the layer

Order 0

Free global energy :

$$\rho_s \psi_s(\underline{u}_1, \underline{u}_2, \alpha) = \int_h w_3(\boldsymbol{\varepsilon}(X + z\underline{n}), \alpha) \rho_3 j(z) dz$$

Thermodynamical forces

$$\underline{T}_{i}^{r} = \rho_{s} \frac{\partial \psi_{s}}{\partial \underline{u}_{i}}, A = -\rho_{s} \frac{\partial \psi_{s}}{\partial \alpha}, G_{h} = -\rho_{s} \frac{\partial \psi_{s}}{\partial h}$$

Global potential of dissipation

$$\rho_s D_s(\underline{v}_1, \underline{v}_2, \dot{\alpha}) = \int_h \rho_3 d_3(\dot{\boldsymbol{\varepsilon}}, \dot{\alpha}) dz$$

Then

$$\underline{T}_i^{ir} = \rho_s \frac{\partial D_s}{\partial \underline{v}_i}, \dots$$

Equilibrium on interface

$$\underline{n}.\boldsymbol{\sigma}j_i = \underline{T}_i^r + \underline{T}_i^{ir}$$

More informations : order 1

The energy depends on $\nabla \underline{u}^o, \underline{w}$, so

$$ho_s \psi_s = f(\underline{u}_i, \nabla \underline{u}_i), \quad
ho_s D_s = g(\underline{v}_i, \nabla \underline{v}_i)$$
 $ho_s = \int_h
ho_3 dz, \text{ Conservation}$

The equilibrium is then obtained as

$$\underline{n}.\boldsymbol{\sigma}j_i = \rho_s \frac{\partial \psi_s}{\partial \underline{u}_i} - \nabla(\rho_s \frac{\partial \psi_s}{\partial \nabla \underline{u}_i}) + \rho_s \frac{\partial D_s}{\partial \underline{v}_i} - \nabla(\rho_s \frac{\partial D_s}{\partial \nabla \underline{v}_i})$$

Example of constitutive laws : f volume fraction of "defects"

$$\psi_s = \frac{1}{2}k(f)(w_n)^2 + \frac{1}{2}\mu(f)(w_t - \alpha)^2$$
$$d(\dot{w}, \dot{\alpha}) = \frac{1}{2}\eta_t(f)\dot{w}_t^2 + \frac{1}{2}\eta_n(f)\dot{w}_n^2 + \frac{1}{2}H(f)\dot{\alpha}^2$$

$$\underline{n}.\boldsymbol{\sigma} = (k_n w_n + \eta_n \dot{w}_n)\underline{n} + (\mu(w_t - \alpha) + \eta_t \dot{w}_t)\tau; \quad A = k_t(w_t - \alpha) = H\dot{\alpha}$$

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Stupkiewicz, Wear (1990),...

Moving punch on a half-space



Rigid Punch on an elastic half space. (Dragon-Louiset,2000)

The interface 3 : fluid + particles.

Suspension of particles in a viscous fluid : $\kappa(c), \quad \eta(c)$

Integral equations on an half elastic space : Galin's Equation

Displacement on the boundary due to stresses on the boundary.

$$\psi_s = \frac{1}{2}\kappa(c)w_n^2, \quad D_s = \frac{1}{2}\eta(c)\dot{w}_t^2$$

Behavior of the interface (3) viscosity in shear

$$\sigma_{xy} = \eta(c)(\dot{u}_x^1 - \dot{u}_x^2), \quad \sigma_{yy} = k(c)(u_y^1 - u_y^2)$$

Galin's Equations for the elastic half space

$$c_{1} u_{x,x}(x) = c_{2} \sigma_{yy}(x) + V p \frac{1}{\pi} \int_{-a}^{a} \frac{\sigma_{xy}(s)}{s - x} ds$$

$$c_{1} u_{y,x}(x) = -c_{2} \sigma_{xy}(x) + V p \frac{1}{\pi} \int_{-a}^{a} \frac{\sigma_{yy}(s)}{s - x} ds$$

$$c_{1} = \frac{E}{2(1 - \nu^{2})}, \quad c_{2} = \frac{(1 - 2\nu)}{2(1 - \nu)}$$

Asymptotic solution for small concentration of particles \boldsymbol{c}

Law $\eta(c)$, $\kappa(c)$.

- order 0 : Hertz contact solution
- order 1 : depends upon criterion of wear : $\phi = \lambda \sigma_{yy}^2$



One more example

Cyclic accommodation for a Cyclic Horizontal motion of a rigid punch



The solution of an half space with a boundary $\eta(x)$

In Galin's Equation, the kernel is changed at order 1 in η .

$$\underline{u}_1(x) = \int_A N_o(x, y) T_1(y) dy + \int_A N_1(x, y) T_o(y) dy$$

The applied loading follows the boundary, using of $D_{\phi}({m \sigma}.\underline{n})$ leads to

$$D_{\phi}(\boldsymbol{\sigma}.\underline{n}) = \dot{\boldsymbol{\sigma}}.\underline{n} + \frac{\mathrm{d}}{\mathrm{d}s}(\eta\boldsymbol{\sigma}.\tau) + \gamma\phi\boldsymbol{\sigma}.\underline{n}$$

1 Asymptotic Respons

- Final State : $\eta(x)$
- Control Variable η
- Cost function (dissipation) J

$$J = \int_{\Gamma} |\eta| dx + a \int_{T} \int_{\Gamma} \langle G(\eta, x, t) - G_c \rangle_{+}^2 dx dt$$

Results

Lost of matter : $\int_{\Gamma} |\eta(x)| dx$





Possibility of using homogeneization technics to describe wear contact and to propose wear laws.

The mass density in the interface is a important internal parameter.

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