



SI-121 1279 Custom Coefficients CRBasic

22-Oct-2008

Calibration Date:

2.41E+09 2.96E+07 00 -2.79E+06 1.64E+07 ပ 72471.2 97544.5 m(SB) b(SB)

Calibration Date:

H(SB)

K(SB)

Use these coefficients under "Declare Constants" section in the example Campbell Scientific datalogger program

instruments

C2

0.00935057

-1.60764



SI-121 1279 Custom Coefficients EdLog

Calibration Date:

30-Apr-2008

	C2	C1	00
m(SB)	0.97545	163.75064	24132.14132
b(SB)	0.72472	-27.94748	-296.26996

142.763 0.00152106 0.145395 P(SB) These coefficients will replace the standard coefficients in commands 3-5 of the example program

SI-322 1090 Custom Coefficients

31-Jul-08

C1 0.294573

121.844

C0

-81.2689 6737.34

# **Specifications**

Field of view Output

Accuracy

Target temp.

from sensor body

0-2500 mV Sensor body temp. -10 to 65 °C

-40 to 70 °C

Optics Wavelength range Response time Input power

Operating environment

Datalogger channels

Cable

Warranty

Precision

22° half angle 60 μV per °C difference

±0.2 °C absolute accuracy ±0.1 °C uniformity ±0.05 °C repeatability ±0.5 °C absolute accuracy

±0.3 °C uniformity ±0.1 °C repeatability and uniformity

8-14 µm (corresponds to atmospheric window) < 1 second to changes in target temperature

2.5 V excitation

-55 to 80 °C; 0 to 100 % RH (non-condensing) Water resistant, designed for continuous outdoor use 1 differential (detector) and 1 single-ended (thermistor)

Precision Narrow

from sensor body

40 µV per °C difference

18° half angle

0-2500 mV

4.5 meters twisted, shielded 4 conductor wire with Santoprene casing. Extra cable \$2.95 per meter.

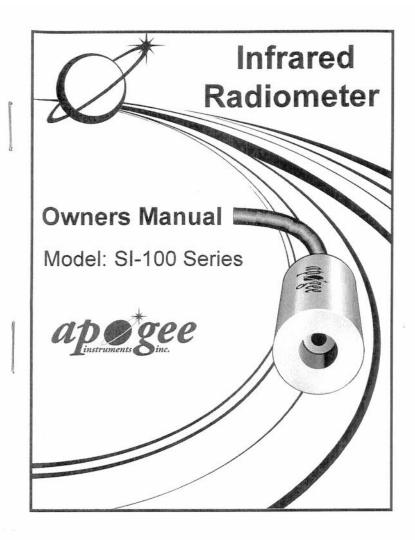
6 cm long by 2.3 cm diameter

1 year against defects in materials and workmanship

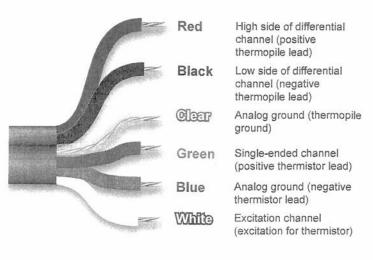


435-792-4700 www.apogeeinstruments.com techsupport@apogee-inst.com

8



### Wiring Diagram

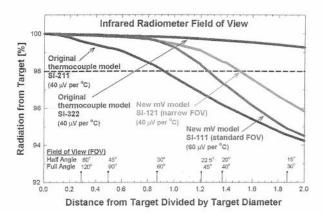


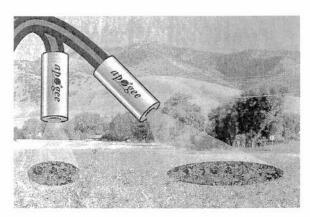
sample programming and instructions available online: www.apogee-inst.com/programs

## Field of View

**Field of View** (FOV) is reported as the halfangle of the apex of the cone formed by the target (cone base) and the detector (cone apex). The target is a circle from which 98% of the radiation being viewed by the detector is being emitted.

Model SI-111 half-angle = 22.0° Model SI-121 half-angle = 18.0°





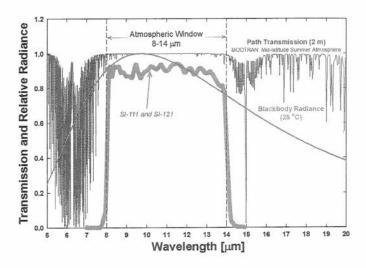
## Mounting

The sensor's FOV (22° or 18°) determines the size of the target area viewed by the detector. This is also influenced by the height and angle at which you mount your IRR. The FOV extends unbroken until it reaches a solid target. Check to be sure you are not detecting unwanted areas within your target diameter, such as the sky.



## **About the Atmospheric Window**

The 8-14  $\mu m$  window of the IRR models corresponds to the atmospheric window. This minimizes the effects of water bands below 8  $\mu m$  and above 14  $\mu m$ .



5

### **Accuracy and Calibration**

During calibration the sensor body temperature ranges from -5 to 45 °C at 10 °C increments. At each step the target temperature ranges from +20 to -15 °C relative to the sensor body temperature.

The output of IRR sensors follows the fundamental physics of the Stefan-Boltzmann Law, which states that radiation transfer is proportional to temperature raised to the fourth power (T). A version of the S-B equation proposed by Kalma et al. (Calibration of small infra-red surface temperature transducers, Ag. For. Met., 1988) is used to calibrate the sensors taking into account the effect of sensor body temperature (see graph shown aboveright):

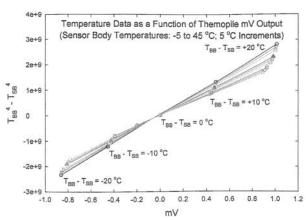
$$T_T^4 - T_D^4 = m \cdot mV + b$$

where  $T_T$  [K] is the target temperature (blackbody cone temperature during calibration),  $T_D$  [K] is the detector temperature, mV is the millivolt output of the detector and serves as a surrogate for emitted energy, m is the slope and b is the intercept. The coefficients m and b are derived during sensor calibration and are functions of the detector temperature.

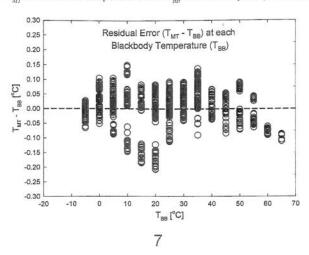
To make temperature measurements, the equation can be rearranged to solve for  $T_T$ , which is calculated from the measured values of  $T_D$  and mV, and the calculated values of m and b (calculated from  $T_D$ ):

$$T_T = (T_D^4 + m \cdot mV + b)^{1/4}$$

6



The graph below shows the residual error  $(T_{\rm MT}-T_{\rm BB})$  where  $T_{\rm MT}$  is measured temperature and  $T_{\rm BB}$  is blackbody temperature).



#### Instructions for measuring and linearizing an Apogee Instruments precision infrared thermocouple sensor in a Campbell Scientific Inc (CSI) datalogger

#### Standard H, K and P Coefficients

Aug. 14, 2003

The equation being implemented is: SEC =  $0.25/Psb^{{(AppTarget T - Hsb)}^{2}}$ -Ksb] (see the original manuscript for derivation).

These instructions can be used in a subroutine for multiple sensors. The reference temperature (referenceT) for all thermocouples must first be measured as specified in the CSI multiplexer manual. The location numbers used in this example (10, 20, 30, 40, 110, 120, and 130) are arbitrary and can be changed.

#### Measure the apparent target temperature (output lead with the black band):

- 1: Thermocouple Temp (differential) (P14)
  - 1:1 Rep
  - 2: 21 2.5 mV 60 Hz Rejection Range
  - 3: 1 IN Channel
  - 4: 3 Type K (Chromel-Alumel)
  - 5: 1 REF TEMP LOC [referenceT]
    6: 10 LOC [AppTargetT]

  - Multiplier 7: 1
  - Offset 8: 0

#### Measure the Sensor Body Temp:

- 2: Thermocouple Temp (DIFF) (P14)
  - 1:1 Rep
  - 2: 21 2.5 mV 60 Hz Rejection Range
  - 3: 2 IN Channel
  - Type K (Chromel-Alumel)
  - REF TEMP LOC [referenceT]
  - 6: 20 LOC [SensorBodyT] 7: 1 Multiplier

  - 8: 0 Offset

### Calculate the P, H, & K Coefficients:

3: Polynomial (P55) (Psb coefficient)

1: 1	Ran
1. 1	Rep

- X Loc [SensorBodyT] 2: 20 CO
- 3: 110 F(X) Loc [Psb]
- 4: 49.9092
- 5: .59237 C1
- C2
- 6: .00558
- (Hsb coefficient) 4: Polynomial (P55)

1	1		

Reps

- 2: 20 X Loc [SensorBodyT]
- F(X) Loc [Hsb] 3: 120
- 4: 4.2828 CO 5: .4248
- 6: -.00077
- C1 C2

- 5: Polynomial (P55) (Ksb coefficient)
  - 1:1 Reps
  - 2: 20 X Loc [SensorBodyT]
  - 3: 130 F(X) Loc [Ksb]
  - 4: 52.0705 CO
  - C1 5: -5.3816
  - C2 6: .387

#### Calculate the sensor error correction factor (SEC) to correct for sensor body temperature:

- 6: Z=1/X (P42)
- {1/Psb} X Loc [Psb] 1: 110
  - Z Loc Psbi 2: 110
- {0.25/Psb} 7: Z=X\*F (P37)
  - X Loc [Psb] 1: 110
    - 2: 0.25
    - 3: 110 Z Loc [Psb]
- {ATT Hsb}
  X Loc [AppTargetT] 8: Z=X-Y (P35)
  - 1: 10
  - 2: 120 Y Loc [Hsb]
  - Z Loc [Hsb] 3: 120
- {ATT Hsb}<sup>2</sup> X Loc [Hsb] 9: Z=X\*Y (P36)
  - 1: 120

  - 2: 120 Y Loc [Hsb]
  - 3: 120 Z Loc [Hsb]
- 10: Z=X-Y (P35) {subtract Ksb}
  - 1: 120 X Loc [Hsb] 2: 130 Y Loc [Ksb]
  - 3: 130 Z Loc [Ksb]
- {calculate SEC} 11: Z=X\*Y (P36) 1: 110 X Loc [Psb]
  - 2: 130 Y Loc [Ksb]
  - 3: 30 Z Loc [SEC]

#### Finally, calculate the corrected target temperature (CTT):

- 12: Z=X-Y (P35) {AppTarget T - SEC} X Loc [AppTargetT]
  Y Loc [SEC] 1: 10
  - 2: 30
  - 3: 40 Z Loc [CTT]